

# MECHANICAL PROPERTIES OF ANODIC TITANIUM DIOXIDE NANOSTRUCTURES

## MEHANSKE LASTNOSTI NANOSTRUKTUR TITANOVEGA DIOKSIDA

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Highly ordered and uniform titanium dioxide (TiO<sub>2</sub>) nanotubes (NTs) with different morphologies (15 nm, 50 nm and 100 nm in diameter) were prepared by the electrochemical anodization of Ti substrates. The TiO<sub>2</sub> NTs' surface properties were characterized by X-ray diffraction (XRD) spectroscopy, Raman spectroscopy, scanning electron microscopy (SEM) and atomic force microscopy (AFM). The elastic modulus (*E*) and the Vickers hardness (HV) of the Ti foil and of the different-morphology TiO<sub>2</sub> NTs were evaluated with the nano-indentation technique. *E* and HV increase with the decreasing length/diameter of the NTs, meaning that NTs with smaller diameters are more resistant to mechanical wear. The elastic modulus of the TiO<sub>2</sub> NTs with 15-nm and 50-nm diameters is similar to that of the human bone.

Keywords: titanium dioxide (TiO<sub>2</sub>) nanotubes, mechanical properties, elastic modulus, Vickers hardness

Z elektrokemično anodizacijo titanovega (Ti) substrata smo pripravili nanocevkke iz titanovega dioksida (TiO<sub>2</sub>) z različno morfologijo. Pripravljene TiO<sub>2</sub> nanocevkke smo karakterizirali z rentgensko difrakcijsko spektroskopijo (XRD), Ramansko spektroskopijo, vrstično elektronsko mikroskopijo (SEM) in mikroskopijo na atomsko silo (AFM). Elastični modul (*E*) in Vickersova trdota (HV) Ti folije in TiO<sub>2</sub> nanocevk z različno morfologijo, sta bili določeni s tehniko nanoindentacije. Elastični modul in Vickersova trdota naraščata z zmanjšanjem dolžine/premera TiO<sub>2</sub> nanocevk, kar pomeni, da so nanocevkke z nižjim premerom bolj odporne na mehansko obrabo. Elastični modul TiO<sub>2</sub> nanocevk, s premerom 15 nm in 50 nm, je podoben elastičnemu modulu človeških kosti.

Ključne besede: nanocevkke iz titanovega dioksida (TiO<sub>2</sub>), mehanske lastnosti, elastični modul, Vickersova trdota

## 1 INTRODUCTION

Titanium and its alloys are some of the most widely used implant materials because of their low toxicity, biocompatibility and mechanical properties. This is attributed to great tensile strength, resistance to body fluid effects, flexibility and high corrosion resistance.<sup>1</sup> Although orthopaedic implants made of titanium alloys imply better results, the limited lifetime of these implants remains a major drawback. This limitation is due to the integration of the Ti-implant material with the juxtaposed bone tissue (osseointegration).<sup>2,3</sup> To overcome osseointegration, the surface of titanium and its alloys can be modified to support cell adhesion and to encourage the formation of new bone at the interface between the implant surface and the bone tissue.<sup>4</sup>

Surface modification involves shifting topography from the micro to nanoscale or tailoring the nanoscale morphology so that the implant surface mimics the feature size of natural tissues and promotes cellular functions.<sup>5,6</sup> Fabricating implant surfaces to have nanoscale dimensions is important because the feature size of all tissues is in the nano regime. For example, natural bone has inorganic constituent made up of 2–5 nm thickness and 20–25 nm wide hydroxyapatite crystals.<sup>7</sup> Electrochemical anodization is one of the most cost-effective and convenient methods of nanoscaling the surface,<sup>8–10</sup> which when performed under self-organized conditions results in TiO<sub>2</sub> NTs grown directly on the Ti substrate material.<sup>1–9</sup> In addition, the morphology of the nanotubes can be tailored for the desired application, e.g., the thickness of these layers can reach several hundreds of μm, while the nanotube diameter can be adjusted from 10 nm to 800 nm.<sup>1,11</sup> Among all the other properties of TiO<sub>2</sub> nanostructures, the elastic modulus is a property that affects directly the implant stability. It is desirable that the

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metal's elastic modulus be as close as possible to that of the bone, because smaller differences between these values will result in a better transfer of stress, and avoiding the stress-shielding effect.<sup>12</sup>

The elastic modulus and hardness of the TiO<sub>2</sub> NTs layer plays an important role for the long-term stability of the implant – the most suitable technique to determine the elastic modulus of such thin TiO<sub>2</sub> oxide layers is nano-indentation. However, the initial roughness and the probe geometry impose limitations. G. A. Crawford et al.<sup>13</sup> have examined the deformation behaviour of a nanotube layer using nano-indentation tests with a Berkovich probe, that led to an indentation penetration higher than the thickness of the nanotube layer and wear marks on the indentation. B. Voltrova et al.<sup>14</sup> studied the influence of the TiO<sub>2</sub> nanotubes' diameter on the nanomechanical properties and found that a larger diameter of the nanotubes showed a lower elastic modulus and indentation hardness, and indicated that TiO<sub>2</sub> nanotubes with a diameter close to 66 nm show the highest in-vitro benefits and therefore could be applied to improve bone implants' osseointegration.

In the present study, TiO<sub>2</sub> NTs with different morphologies were obtained by using electrochemical anodization and the nano-indentation properties of different diameter nanotubes were studied based on the Oliver-Pharzz methodology.

## 2 EXPERIMENTAL PART

### 2.1 Materials

Titanium foil (Advent Research Materials, 0.1 mm thickness, 99.6 %), ethylene glycol (Fluka, ≥99.5 %), ammonium fluoride – NH<sub>4</sub>F (Sigma Aldrich, 28.0–30.0 %), hydrofluoric acid – HF (Sigma Aldrich, ≥40 %) acetone (Honeywell Riedel – de Haen, 99.5 %), ethanol (Sigma Aldrich, 96%), deionized water (miliQ).

### 2.2 Fabrication of TiO<sub>2</sub> nanosurfaces

The fabrication of the TiO<sub>2</sub> NTs was carried out according to the electrochemical anodization method as in references,<sup>5–8</sup> although using slightly different parameters, as described below. All the anodization experiments were carried out at room temperature (~20 °C) in a two-electrode system, using Ti foil as the working electrode and a platinum gauze as the counter electrode. Prior to anodization, the Ti foils were degreased by successive ultrasonication in acetone, ethanol and deionised water for 5 min each and dried in a nitrogen stream. An ethylene glycol-based electrolyte containing NH<sub>4</sub>F (0.35 w/w%) and H<sub>2</sub>O (1.7 w/w%) was used to grow the TiO<sub>2</sub> NTs. This step was followed by removing the nanotubular layer via ultrasonication in deionised water and then by drying the pre-patterned sample in a nitrogen stream. This pre-patterned surface was subsequently used as a substrate in the anodization in the ethylene-gly-

col-based electrolyte containing hydrofluoric acid (**Table 1**), used to grow homogeneous layers of self-arranged TiO<sub>2</sub> NTs. The as-formed TiO<sub>2</sub> NTs were immersed in ethanol for 2 h in order to remove the organic components from the electrolyte solution.

## 2.3 Surface characterization of Ti nanostructures

### 2.3.1 Scanning Electron Microscopy (SEM)

The morphology of the TiO<sub>2</sub> nanostructures was observed using a field-emission scanning electron microscope – Hitachi FE-SEM S4800.

### 2.3.2 Atomic Force Microscopy (AFM)

Topographic features of the Ti foil and of the 100-nm-diameter TiO<sub>2</sub> NTs were studied by Atomic Force Microscopy (Solver PRO, NT-MDT, Russia) in tapping mode in an air atmosphere. The samples were scanned with the standard Si cantilever (MikroMasch) at a constant force of 22 N/m and resonance frequency of 325 kHz (10 nm tip radius and 95 μm tip length). The average surface roughness ( $R_a$ ) was calculated from 10 different images made on (5×5) μm areas.

### 2.3.3 Scanning Probe Microscopy (SPM)

The 3D topography of the titanium substrate surface was obtained by Hysitron's *in-situ* Scanning Probe Microscopy (SPM). Samples were scanned at a contact force of 1 μN between a nano-indentation tip (diamond Berkovich) and a titanium substrate surface. *In-situ* SPM images were analysed using Hysitron's TriboView™ software. The average surface roughness ( $R_a$ ) was calculated from a (20×20) μm area. 3D topography of the TiO<sub>2</sub> NTs' surface was obtained by Hysitron's *in-situ* SPM as well. Samples were scanned at a contact force of 0.05 μN between the nano-indentation tip (diamond Cube Corner) and the TiO<sub>2</sub> NTs' surface.

### 2.3.4 Raman spectroscopy

Raman spectra of all TiO<sub>2</sub> samples were recorded using a Horiba Jobin-Yvon LabRAM HR800 Raman spectrometer equipped with 100× optical microscope, appropriate holographic notch filters and 1800 grooves/mm holographic grating to provide the spectral resolution of 0.25 cm<sup>-1</sup>. A 632.8 nm helium-neon laser of 10-mW power and 2-μm spot size was used to excite the samples. The spectra were taken in the wavenumber range of 100–1000 cm<sup>-1</sup> with an exposure time of 2s.

### 2.3.5 X-ray diffraction analysis (XRD)

The crystal structure of the nanotube arrays was also confirmed using X-ray diffraction (XRD; PAN analytical D8 model) with Cu-K<sub>α</sub> radiation ( $K_{\alpha} = 0,15400$  nm) in the  $2\theta$  range 20–80.

### 2.3.6 Nanoindentation studies

A Hysitron TI 950 TriboIndenter™ nanomechanical test instrument was used for an assessment of the depth

**Table 1:** Influence of the anodization conditions used on the morphology (diameter and length) of TiO<sub>2</sub> NTs

Diameter (nm)	Electrolyte	Potential (V)	Anodization time (h)	Length (μm)
15	EG+8M H <sub>2</sub> O+0.2M HF	10	2.5	0.22
50	EG+8M H <sub>2</sub> O+0.2M HF	20	2.5	1.10
100	EG+8M H <sub>2</sub> O+0.2M HF	58	2.5	3.50

profiles of the mechanical properties on TiO<sub>2</sub> NTs (diameters 15 nm, 50 nm and 100 nm) and Ti foil as a reference sample. The partial unload approach requires elastic-plastic deformation during gradual force cycles in order to analyse each unloading segment according to the Oliver & Pharr method<sup>15</sup>. Automated analysis plots the depth profile as discrete datasets. Based on the 1/10 rule, a coating of 100-nm thickness requires measurements at <10 nm depth.<sup>16</sup> A standard Berkovich tip area function  $A(h)$ , describing the shape of the indentation probe, was used:  $A = 24.5h^2 + C1h + C2h^{1/2} + C3h^{1/4} + C4h^{1/8} + C5h^{1/16}$ , where  $C1 = 7.6736E+3$ ,  $C2 = -2.3046E+5$ ,  $C3 = 1.9088E+6$ ,  $C4 = -4.2845E+6$  and  $C5 = 2.6127E+6$ . A Ti foil was used as reference to examine the nano-mechanical properties of TiO<sub>2</sub> NTs with diameters of 15 nm, 50 nm and 100 nm.

**Table 2:** Number of TiO<sub>2</sub> NTs in the contact with the Berkovich tip for contact depth  $hc = 5$  nm and  $hc = 35$  nm corresponding to the diagram in Figure 1 calculated from tip area function

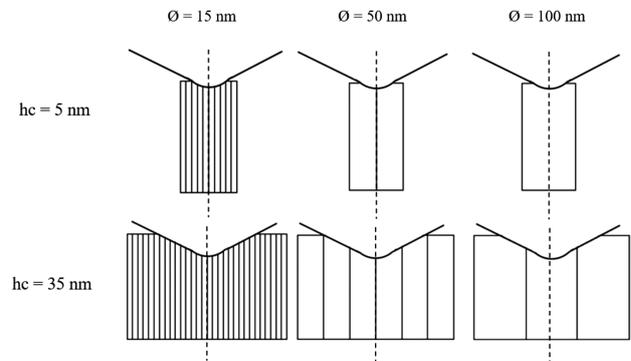
Diameter (nm)	TiO <sub>2</sub> NTs in the contact $hc = 5$ nm (quantity)	TiO <sub>2</sub> NTs in the contact $hc = 35$ nm (quantity)
15	39.44	224.56
50	3.55	20.21
100	0.89	5.05

### 3 RESULTS

#### 3.1 Morphology of TiO<sub>2</sub> NTs

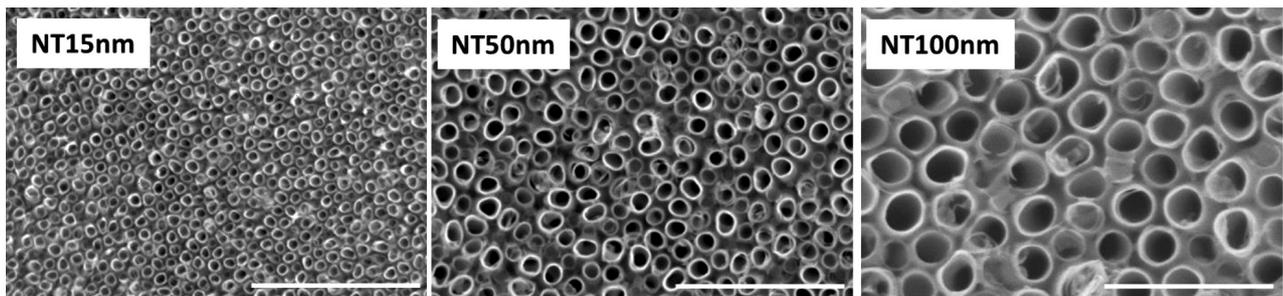
The morphology of the TiO<sub>2</sub> NTs was evaluated with SEM. Analyses indicate the different diameters of the TiO<sub>2</sub> NTs (Figure 2), i.e., 15 nm, 50 nm and 100 nm with standard deviations of 20 %, 10 % and 5 %, respectively, that were achieved by changing the anodization potential used in the electrochemical anodization (Table 1).

The topographical features of the Ti foil used as a substrate for the growth of NTs, as well as of the TiO<sub>2</sub> NTs with 100 nm diameter were investigated by AFM,

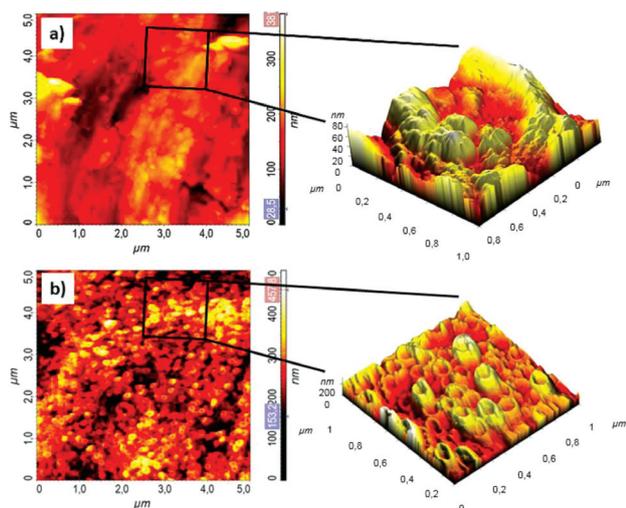


**Figure 1:** Schematic representation of contacts of the Berkovich indenter and TiO<sub>2</sub> NTs in the nano-indentation test

as presented in Figure 3. The AFM analysis of Ti foil shows that the surface is not fully uniform, and some vertical distortions (vertical roughness) are observed with the AFM (Figure 3a). The average surface roughness measured on a (5×5) μm area was about 35 nm. On the surface of the 100-nm-diameter TiO<sub>2</sub> NTs, features were clearly observed with the AFM, as the size of the nanotube diameter was sufficiently wide to enable the tip penetration inside the hollow nanotube interior, which was not possible for TiO<sub>2</sub> NTs with a smaller diameter, such as the TiO<sub>2</sub> NTs with 15 nm in diameter and TiO<sub>2</sub> NTs with a 50 nm in diameter. The average roughness measured on a (5×5) μm area for TiO<sub>2</sub> NTs with 100 nm in diameter was about 47 nm. However, it should be noted that this value is not entirely representative, as the AFM tip could only enter up to a limited length of the nanotube (as previously shown (8), the length of the TiO<sub>2</sub> NTs with 100 nm in diameter is about 3.5 μm as evaluated from SEM analysis). More importantly, the AFM results clearly show the opened hollow structure of the TiO<sub>2</sub> NTs as well as the slight deviations in their height, about 200 nm, as observed from the 3D image (Figure 3b).



**Figure 2:** SEM images of the top surface of TiO<sub>2</sub> NTs (size of the scale bar=500 nm)

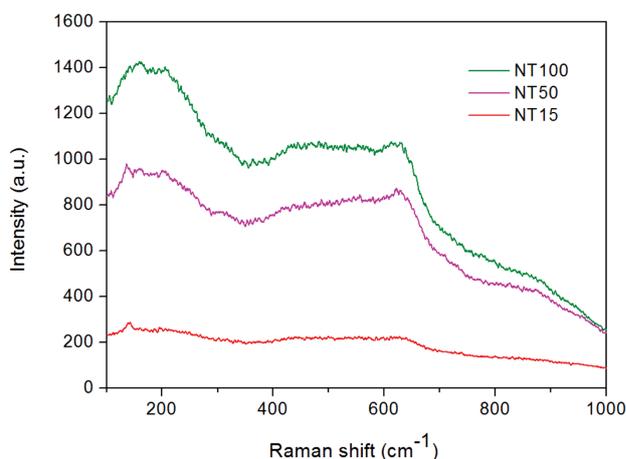


**Figure 3:** AFM images of: a) Ti foil, b) TiO<sub>2</sub> NTs with 100 nm in diameter. Zoomed region (along vertical z-direction) shows further topological details

The 3D topography of the titanium substrate (Ti foil) surface is also obtained by *in-situ* SPM, see **Figure 4a** and shows a non-negligible roughness of the sample. The average roughness of the Ti substrate surface was around 49 nm. Similarly, **Figures 4b** and **4c** show the *in-situ* SPM images of 100-nm-diameter TiO<sub>2</sub> nanotubes surface.

### 3.1.1 Crystal structure of TiO<sub>2</sub> NTs

Raman spectroscopy provides very important information about the Raman-active vibrational modes related to the Ti-Ti, Ti-O and O-O bonds in TiO<sub>2</sub>. It is well known that anatase TiO<sub>2</sub> gives a strong Raman signal at 144 cm<sup>-1</sup> followed by low intensity peaks at (197, 394-399, 513/514, 519 and 635-641) cm<sup>-1</sup>, whereas rutile TiO<sub>2</sub> gives Raman signals at 143, 236/242, 446/447 and 610/613 cm<sup>-1</sup>.<sup>17-19</sup> The Raman spectra for all TiO<sub>2</sub> samples of different diameters are presented in **Figure 5**. All the spectra show broad bands and no clear spectral characteristics of anatase or the rutile phase of TiO<sub>2</sub>. Thus, the TiO<sub>2</sub> nanotubes produced in our electrochemical anodization process are of an amorphous nature.<sup>20</sup> The broad bands appearing near 284 cm<sup>-1</sup> and in the



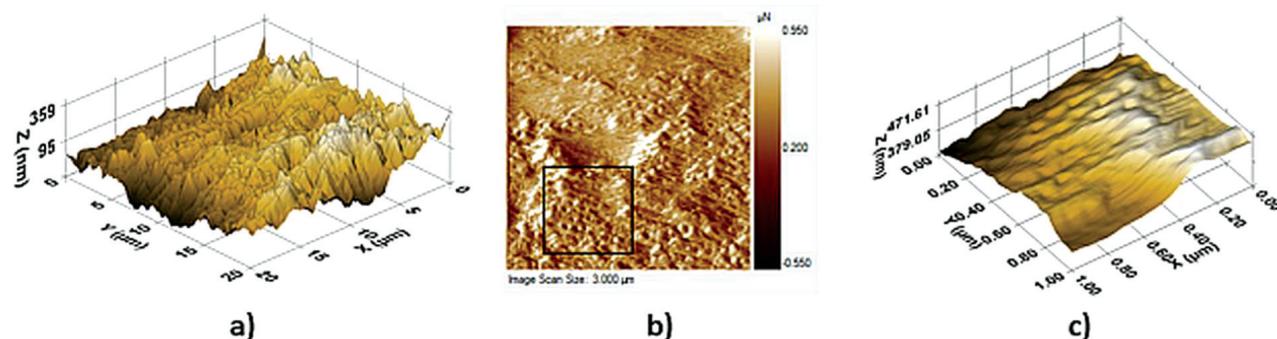
**Figure 5:** Raman spectra of TiO<sub>2</sub> NTs with various diameters. T=Ti substrate

range 430–630 cm<sup>-1</sup> in all the spectra can be assigned to O–O interactions consistent with the TiO<sub>6</sub><sup>8-</sup> octahedral structure and the Ti-O interactions, respectively.<sup>(19)</sup> A sharp peak appearing at 143/144 cm<sup>-1</sup> in the spectrum of the TiO<sub>2</sub> NTs with 15-nm diameter can be considered to arise from slightly rutile/anatase phase of TiO<sub>2</sub> nanotubes due to Ti–Ti covalent interactions. This feature tends to cease, and the amorphous nature tends to be more prominent as the tube diameter increases to 50 nm and 100 nm. The weak band near 840 cm<sup>-1</sup> can be assigned as the first overtone of the 143/144 cm<sup>-1</sup> band.<sup>21</sup>

The XRD patterns for the different diameter as-grown TiO<sub>2</sub> NT arrays as well as for the substrate material (Ti foil) are presented in **Figure 6**. After the electrochemical anodization, no crystalline phase is detected for the as-grown NTs, thus further confirming their amorphous state. Comparing the patterns of the TiO<sub>2</sub> NTs with that of the substrate materials only peaks characteristic for the Ti substrate materials are detected. These results are in agreement with the previous report.<sup>22</sup>

### 3.1.2 Nanoindentation studies

The mechanical stability of the implant is an essential factor to maintain its long-term success. In the present study, the mechanical properties of TiO<sub>2</sub> NTs with differ-



**Figure 4:** *In-situ* SPM images: a) 3D topography of titanium foil, b) map of gradients of forces obtained from TiO<sub>2</sub> NTs with 100 nm in diameter sample and c) 3D topography of the area demarcated by a black square in the picture from b)

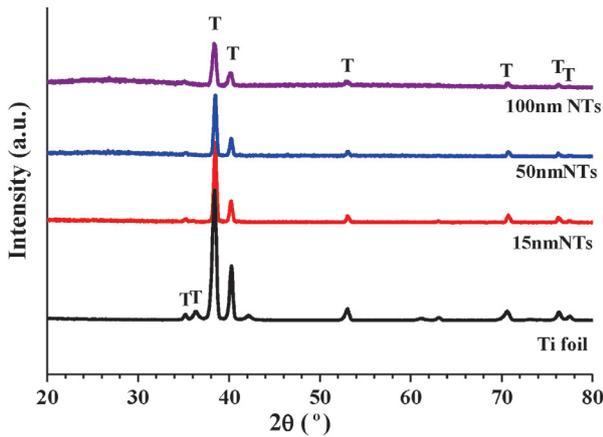


Figure 6: X-ray diffraction (XRD) patterns of Ti substrate and TiO<sub>2</sub> NTs with various diameters (T=Ti substrate)

ent lengths and diameters (Table 1) were measured with a Berkovich indenter. Values of *E* and *HV* (calculated from apparent indentation hardness *HIT*) were calibrated from contact depths *hc* = 5 nm and *hc* = 35 nm, respectively (Figure 7).<sup>16</sup>

In this work, the elastic modulus increases with decreasing diameter of the TiO<sub>2</sub> NTs, and with decreasing length as well. The evaluated *E* is 8.7±4.2 GPa for TiO<sub>2</sub> NTs with 100 nm in diameter, 10.3±4.6 GPa for TiO<sub>2</sub> NTs with 50 nm in diameter and 19.2±4.3 GPa for TiO<sub>2</sub> NTs with 15 nm in diameter (Figure 8). Y.N. Xu et al.<sup>23</sup> reported an elastic modulus of 5.1 GPa for longer TiO<sub>2</sub> NTs (~8.5 μm), with a diameter of ~199 nm and a wall thickness of ~14.3 nm. However, the elastic modulus of the 15-nm- and 50-nm-diameter TiO<sub>2</sub> NTs evaluated in the present study is similar to that of bone, which is 11–30 GPa.<sup>24</sup>

It has been reported that the hardness of films is dependent on their adhesion to the substrate, i.e., the higher the hardness, the higher the adhesion.<sup>25</sup> In present study, *H<sub>v</sub>* increases with decreasing length/diameter of the NTs; therefore, TiO<sub>2</sub> NTs of 15 nm in diameter exhibit the highest adhesion strength to the substrate (Figure 9). Since adhesion is higher for smaller diameter TiO<sub>2</sub> NTs,

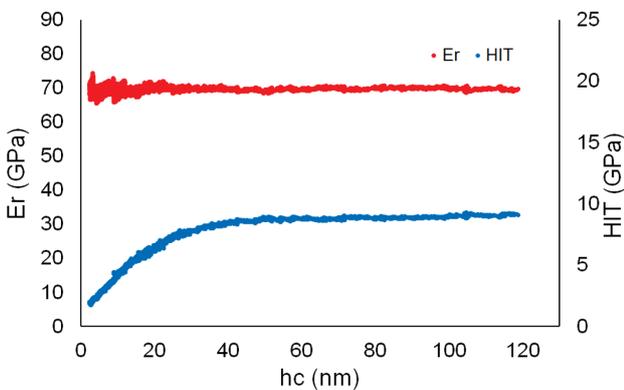


Figure 7: Calibration values of *E* and *H* vs. contact depth on fused quartz sample

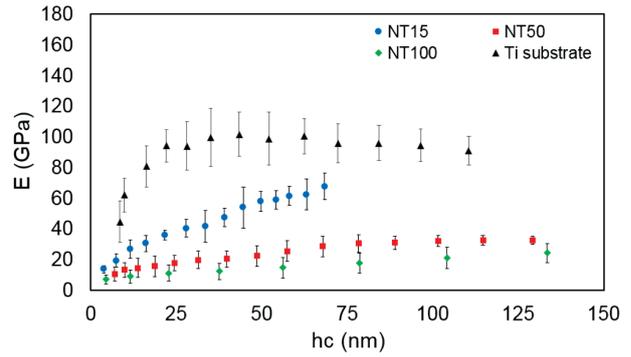


Figure 8: Depth profile of Young's modulus

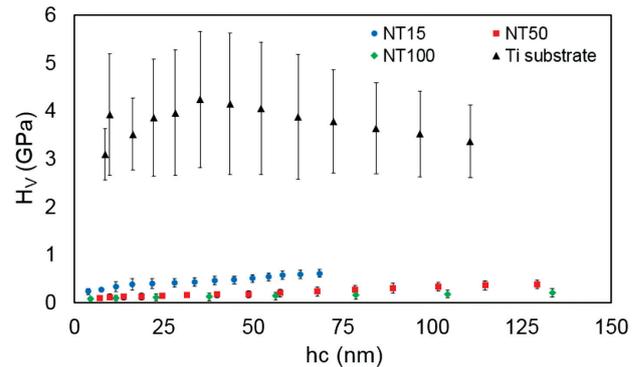


Figure 9: Depth profiles of calculated Vickers hardness. The Vickers hardness was calculated from the measured apparent indentation hardness *H<sub>v</sub>* (GPa) = 0.92666\**HIT*

it follows that such nanostructures are also more resistant to mechanical wear.<sup>26</sup> However, the *H<sub>v</sub>* values are consistent with the existing reported values. For instance, Y. N. Xu et al.<sup>23</sup> reported a hardness of 0.094 GPa for longer TiO<sub>2</sub> NTs (diameter: approx. 199 nm, wall thickness: 1 approx. 14.3 nm and length: approx. 8.5 μm). In the present study, *H<sub>v</sub>* is 0.45±0.09 GPa for TiO<sub>2</sub> NTs with 15 nm in diameter, 0.16±0.06 GPa for TiO<sub>2</sub> NTs with 50 nm in diameter and 0.12±0.08 GPa for TiO<sub>2</sub> NTs with 100 nm in diameter. The average *H<sub>v</sub>* of the Ti foil is 3.8 ±0.3 GPa.

#### 4 CONCLUSIONS

Amorphous, as-formed TiO<sub>2</sub> NTs with diameters of 15 nm, 50 nm and 100 nm were prepared by electrochemical anodization. The nano-indentation studies revealed that the elastic modulus and Vickers hardness of the TiO<sub>2</sub> NTs increased with the decreasing length/diameter of the TiO<sub>2</sub> NTs (as a reference, a Ti foil was measured). The elastic modulus of 15 nm and 50 nm diameter TiO<sub>2</sub> nanotubes is similar to the elastic modulus of the human bone. The Vickers hardness of the 15-nm-diameter TiO<sub>2</sub> nanotubes exhibits the highest adhesion strength to the substrate. These results indicate that the TiO<sub>2</sub> NTs with smaller diameters are more resistant to mechanical wear. Such materials can be used in medical

applications, such as orthopaedic implants or drug-delivery systems.

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