Calculation of the Thermodynamic Properties in the Ir-B System Based on the Known Phase Diagram

Dragana Živkovič¹, Leonida Stuparević

¹ Technical Faculty VJ 19210 Bor, Serbia and Montenegro; Phone/Fax: ++381 30 424 547; E-mail: dzivkovic@tf.bor.ac.yu

Abstract: The results of the thermodynamic properties calculation in the binary Ir-B system is presented in this paper. Based on the known liquidus and solidus lines from the phase diagram, specific calculation procedure according to Rao and Belton was done, so activities and activity coefficients for iridium and boron were determined at the temperatures of 2800, 2900 and 3000K.

Keywords: alloy thermodynamics, phase diagram, Ir-B system

Received: December 14, 2004 Accepted: September 15, 2005

Introduction

Several investigations on the iridium borides have been reported in literature by Arronson ET AL. in 1962 [1] and 1963 [2], LUNDSTRAM in 1967 [3], ROGL ET AL. in 1971 [4], as well as the

liquidus and solidus-liquidus data according to IPSER AND ROGL in 1981 ^[5] and metalographical investigation of Ir-B system by STUPAREVIĆ in 1986 ^[6].

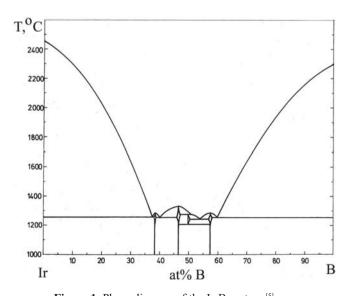


Figure 1. Phase diagram of the Ir-B system [5].

Temperature, °C	Reaction	B-content (at%)	Type of reaction
1259 ± 4	$L \rightarrow Ir + IrB_{0.7}$	37.5	eutectic
1287 ± 4	$L \rightarrow IrB_{0.7}$	38.5	congr. melt.
1258 ± 4	$L \rightarrow IrB_{0.7} + IrB_{0.9}$	40.0	eutectic
1333 ± 4	$L \rightarrow IrB_{0.9}$	46.5	congr. melt.
1274 ± 0	$L + IrB_{0.9} \rightarrow IrB$	50.0	peritectic
1209 ± 3	$IrB \rightarrow IrB_{0.9} + IrB_{1.35}$	50.0	eutectoid
1248 ± 3	$L \rightarrow IrB + IrB_{1.35}$	54.0	eutectic
1287 ± 5	$L \rightarrow IrB_{1.35}$	57.5	congr. melt.
1255 ± 0	$L \rightarrow IrB_{1.35} + B$	60.0	eutectic

Table 1. Characteristic reactions in the Ir-B system according to IPSER AND ROGL [5].

Phase diagram of the Ir-B binary system is given in Fig.1, while the characteristic reactions and their type at the certain compositions and temperatures are presented in Table 1.

Concerning the thermodynamic data for this binary system, there are no adequate references in literature. The main reason for this is the high investigating temperature, which causes many difficulties in the experimental work.

So, as a contribution to the better thermodynamic knowledge of the Ir-B binary system, an analytical approach to this subject is presented in this paper. Based on the known liquidus and solidus lines from the phase diagram, specific calculation procedure according to RAO AND BELTON [7,8] was performed, which enabled the determination of the activities, activity coefficients and other partial molar quantities at the temperature of 2500 K.

THEORETICAL FUNDAMENTALS

In some binary systems it is possible to calculate the activity coefficients of components in liquid solutions from the locations of the liquidus and solidus lines on the phase diagrams. For systems of simple eutectic type, with little or no terminal solid solubility, this method offers a means of obtaining the activity coefficients with acceptable accuracy ^[7,8].

For illustration of this method, two examples of calculation will be given for the imaginary binary eutectic Me₁-Me₂ system (where Me₁ and Me₂ are different metals):

- *first*, if there are no terminal solid solubility, and
- *second*, if there is little solid solubility in the investigated system.

First case: Assume that on the Me₂-rich side of the phase diagram the liquidus descends sharply with increasing Me₁ content and terminates at the eutectic point (T_2, x_{Me^2}) .

Because solid Me_2 dissolves no Me_1 , then, at any point on the liquidus curve, a liquid Me_1 - Me_2 solution of composition x_{Me2} is in equilibrium with pure solid Me_2 , at temperature T. In other words,

$$Me_1$$
- Me_2 (liquid alloy) = Me_2 (pure, solid) at T (1)

The partial molar free energy of Me_2 in the liquid alloy, G_{Me2} , is equal to the molar free energy of the pure solid Me_2 , $G^{\circ}_{Me2(s)}$. Thus

$$G_{Me2} = G_{Me2(1)}^{\circ} + RT \ln a_{Me2}^{\circ} = G_{Me2(s)}^{\circ}$$
 (2)

where a_{Me2} is the activity of Me_2 in the liquid alloy with respect to the pure liquid Me_2 standard state. Rearranging the terms,

$$RTIna_{Me2} = G^{\circ}_{Me2(s)} - G^{\circ}_{Me2(l)} = -\Delta G^{\circ}_{s \to l(Me2)}$$
(3)

where $\Delta G^{\circ}_{s \to l(Me2)}$ is the standard free energy of fusion for Me_2 at temperature T (this quantity should be expressed as a function of temperature using data on heat of fusion and heat capacity).

Second case: In the case of eutectic systems, with little terminal solid solubility of Me₂ in Me₁, following equilibrium reaction could be written:

$$Me_{1}-Me_{2}$$
 (liquid, x_{Me1}^{l}) = $Me_{1}-Me_{2}$ (solid, x_{Me1}^{s}) (4)

which means that activity of Me₁-component is less then 1. Further, this can be expressed as

$$G_{Me(1)} = G_{1(1)}^{\circ} + RT \ln a_{1(1)}^{1} = G_{1(s)} = G_{1(s)}^{\circ} + RT \ln a_{1(s)}$$
(5)

where $a_{Me1(1)}$ and $a_{Me1(s)}$ are activities of Me_1 -component in liquid (related to pure liquid Me_1 in the standard state) and solid phase (related to pure solid Me_1 in the standard state), respectively. When solubility of Me_2 in the Me_1 is not too high, it can be assumed that the solid phase is amenable to Raoult law, so $a_{Me1(s)} = x_{Me1}^s$. Rearranging the Eq. (5) one obtains

$$\log a_{Me1(l)} = \log x_{Me1}^{s} - \Delta G_{s \to l(Me1)}^{o} / 2.303RT$$
 (6)

which is the basic equation for the calculation of $a_{Me1(I)}$ at different liquidus temperatures T. When values for activities of Me_2 - component in liquid alloys of different compositions - at the liquidus temperature are calculated, the activity coefficients at the investigated temperature T' can be calculated assuming regular solution behavior for the melts as follows [8]

$$\gamma' = \gamma_i^{(T/T')} \tag{7}$$

Systems that are amenable to this type of analysis include, for example, lead-silver, iron-silicon, magnesium-silicon, iron-copper, etc. Often, in this type of system, experimental data on activities are available for only a limited range of compositions, and these data can be combined with activity data deduced from the phase diagram [8]. For some systems, Ir-B for example, where no data are available, this method could be very useful in the thermodynamic analysis and obtaining the activity-composition relation for the investigated composition range.

RESULTS AND DISCUSSION

The Ir-B phase diagram belongs to the group of systems for which the described calculation method ^[7,8] could be applied. But, the characteristics of this system make it differ from the original look of the simple eutectic type diagrams: numerous iridium borides occurs in the middle region of the phase diagram ^[5], so concentration range with iridium molar content 0.35-0.65 was not considered.

Regions in the concentration range that were investigated are alloys with $x_{lr} = 0$ -0.35 and 0.6-1, respectively. For the first interval, iridium-rich side was treated and thermodynamic properties for iridium were determined, and in the second interval, boron-rich side of the phase diagram was investigated and thermodynamic properties for boron were determined.

Values of chosen alloy compositions and adequate liquidus temperatures read from the Ir-B phase diagram are shown in Table 2.

Table 2. Chosen compositions and adequate liquidus temperatures.

xIr	хB	T_{liq}, K
0.05	0.95	2503
0.10	0.90	2414
0.15	0.85	2310
0.20	0.80	2184
0.25	0.75	2058
0.30	0.70	1895
0.35	0.65	1732
0.65	0.35	1651
0.70	0.30	1866
0.75	0.25	2058
0.80	0.20	2236
0.85	0.15	2932
0.90	0.10	2532
0.95	0.05	2629

In further analysis, thermodynamic properties for the adequate component were calculated considering the calculation procedure given by Eq. (6). Results of this calculation, which include the value for $\Delta G^{\circ}_{s \rightarrow l}$ for boron and irridium at the corresponding liquidus temperature, the activities and activity coefficients for both components in the liquid phase at the liquidus temperature are presented in Table 3.

Table 3. Results of the thermodynamic calculation at the liquidus temperature.

xIr	$\Delta G^{0}_{s\rightarrow l}(B)$	loga _B	$\mathbf{a}_{\mathbf{B}}$	γв
0.05	0	-0.04576	0.900	0.947
0.10	331	-0.07774	0.836	0.929
0.15	1289	-0.12605	0.748	0.880
0.20	2448	-0.18348	0.655	0.819
0.25	3605	-0.24639	0.567	0.756
0.30	5095	-0.32751	0.470	0.672
0.35	6570	-0.41996	0.380	0.585
xIr	$\Delta \mathbf{G^{o}}_{s \to l}$ (Ir)	$loga_{Ir}$	a_{Ir}	γ_{Ir}
0.65	9608	-0.49102	0.323	0.497
0.70	7877	-0.37537	0.421	0.602
0.75	6201	-0.28231	0.522	0.696
0.80	4573	-0.20372	0.626	0.782
0.85	3106	-0.12591	0.748	0.880
0.90	1770	-0.08227	0.827	0.919
0.95	838	-0.03892	0.914	0.962

The calculation of activities and activity coefficients at the investigated temperatures of 2800, 2900 and 3000K, was done according to Eq. (7), assuming regular solution behavior for the melts. As for the illustration, dependencies of iridium and boron activities on composition at the temperature of 3000K are shown in Fig. 2.

Negative deviation from the Raoult law in the investigated composition ranges could be noticed for both components (γ_{Ir} <1 and γ_{B} <1), which means that good miscibility between

Temp.	2800K		2900K		3000K	
xIr	$\gamma \mathbf{B}$	aB	γB	aB	γΒ	aB
0.05	0.953	0.905	0.954	0.907	0.956	0.908
0.1	0.938	0.845	0.941	0.846	0.942	0.848
0.15	0.900	0.765	0.903	0.768	0.906	0.770
0.2	0.856	0.685	0.861	0.688	0.865	0.692
0.25	0.814	0.611	0.820	0.615	0.825	0.619
0.3	0.764	0.535	0.771	0.540	0.778	0.545
0.35	0.718	0.467	0.726	0.472	0.734	0.477
0.4	0.924	0.554	0.927	0.556	0.929	0.557
xIr	γIr	aIr	γIr	aIr	γIr	aIr
0.65	0.662	0.430	0.671	0.436	0.680	0.442
0.7	0.713	0.499	0.721	0.505	0.729	0.510
0.75	0.766	0.575	0.773	0.580	0.780	0.585
0.8	0.822	0.657	0.827	0.662	0.833	0.666
0.85	0.875	0.744	0.879	0.747	0.883	0.750
0.9	0.927	0.834	0.929	0.836	0.932	0.838
0.95	0.965	0.916	0.966	0.918	0.967	0.919

Table 4. Thermodynamic properties for iridium and boron at the investigated temperature.

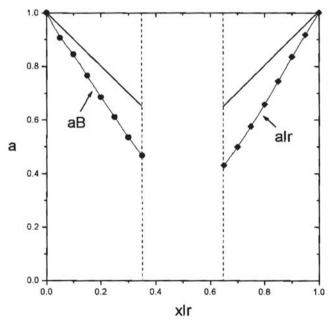


Figure 2. Dependencies of iridium and boron activities on the composition at 3000K.

constitutional components in the iridiumboron system exists. This fact is in agreement with the phase diagram type, in which numerous iridium borides are formed. Also, it could be noticed that the activity value increases with increasing temperature, coming closer to the Raoult line. Having in mind that, up to now, there were no thermodynamic properties on this system, as well as the fact that extremely high temperatures were taken into the consideration, the application of the Rao and Belton's calculation procedure could be very useful and adequate methodology for thermodynamic investigation of such systems.

REFERENCES

- [1] Aronsson, B., Stenberg, E., Aselius, J. (1962): *Nature* 195, p. 377.
- [2] Aronsson, B., (1963): *Acta Chem. Scand.* 17, p. 2036.
- [3] LUNDSTRAM, T. (1967): *Coll. Int. du CN RS* 157, p. 91.
- [4] ROGL, P., NOWATNY, H., BENESOWSKY, F. (1971): *Monatsh. Chem.* 102, p. 678.
- ^[5] IPSER, H., ROGL, P. (1981): *J. Less Comm. Met.* 82, p. 363.
- [6] STUPAREVIĆ, L (1986): Coll. Papers 22(2),217 p. (in Serbian).
- [7] RAO, Y.K., BELTON, G.R. (1981): In Chemical Metallurgy A Tribute to Carl Wagner; Edited by N.A. Gocken, pp.75-96, *Metall.Soc. of AIME*, Warrendale, Pa.
- [8] RAO, Y.K. (1985): Stoichiometry and Thermodynamics of Metallurgical Processes, Cambridge University Press, New York.